WIRELESS USER TERMINAL AND SYSTEM HAVING HIGH SPEED, HIGH RESOLUTION, DIGITAL-TO ANALOG CONVERTER WITH OFF-LINE SIGMA DELTA CONVERSION AND STORAGE

5 ## Cross Reference to Related Applications

This invention is related to copending applications: (TI-32886), Serial No. _____, filed _____; (TI-32956), Serial No. _____, filed _____; and (TI-32957), Serial No. _____, filed _____, all of

10 which are herein incorporated by reference.

Technical Field of the Invention

15 This invention pertains to a wireless user terminal and corresponding system that incorporate a digital-to-analog (D/A) converter for performing high speed and high-resolution digital-to-analog conversion using an oversampling principle.

20 ## Background of the Invention

Digital-to-analog conversion refers to the process of converting discrete digital signals into a continuous-time range of analog signals. The conversion of analog signals to digital signals and vice versa is often used in order to interface real world systems,

25 many of which monitor continuously varying analog signals, with digital systems that read, store, interpret, manipulate and otherwise process the discrete values of sampled analog signals. Real world applications which use digital-to-analog converters (DACs) include, for example, digital audio systems such as compact disc players, digital video players, and various other high performance audio applications, which include conversion

30 of digital signals to analog waveforms at a high resolution.

5   Sigma-delta modulation (sometimes called "delta-sigma modulation") provides a
high-resolution digital-to-analog conversion solution. Sigma-delta DACs have come into
widespread use with the development of signal processing and digital audio technologies
and their applications. Sigma-delta modulation incorporates a noise-shaping technique
10   whereby the noise of a quantizer (often 1-bit) operating at a frequency much greater than
the bandwidth is moved to high frequencies not of interest in the output signal. A filter
after the quantizer removes the out-of-band noise. The resulting system synthesizes a
high-resolution data converter, but is constructed from low-resolution building blocks.
Since sigma-delta DACs provide for oversampling digital-to-analog conversion through
15   the sampling of signals at very high frequencies (i.e., sampling at rates much greater than
the Nyquist rate), high signal-to-noise ratios are achieved. Thus, the combination of
oversampling and noise shaping technologies may be implemented using a sigma-delta
DAC in order to achieve high resolution without external trimming. There, however,
does not exist at present a digital-to-analog conversion solution that provides both high
20   speed and high resolution. A good overview of the theory of sigma-delta modulation is
given in "Oversampling Delta-Sigma Data Converters," by Candy and Temes, IEEE
Press, 1992. Examples of D/A converters utilizing delta-sigma modulation are given in
U.S. Patent Nos. 4,901,077; 5,079,551; 5,185,102; 5,313,205; 5,701,106; 5,712,635;
5,786,779; 5,920,273; and 5,952,947. The disclosures of the foregoing references are
25   incorporated herein by reference.

          Specifically, sigma-delta DACs commonly include a front-end interpolator which
receives digital input samples and increases the sampling rate (typically 64 - 256 times
the input sample rate) of the digital input samples. The sigma-delta modulator receives
30   the higher frequency input samples from the interpolator and converts the samples to a
lower resolution (typical one-bit), high frequency bit stream. Rather than spreading
quantization noise uniformly over the frequency range from 0 to the sampling Nyquist
frequency, the sigma delta modulator shapes the noise so that the majority of the noise
falls into the very high frequencies above the Nyquist frequency. Thus, it effectively

5   removes the noise from the lower frequency range which is of interest for the particular
applications cited above. Techniques for increasing the sample rate, generally called
interpolation, are well understood by those skilled in the art. Most designs will utilize
several stages of increase.

10   An oversampling DAC which utilizes a second order sigma-delta quantizer and an
analog low pass filter to convert the data from the sigma-delta quantizer to analog signal
is a very effective device for low speed audio applications; yet, inadequate for high speed
applications. In addition, it has a relatively high output data transition rate, requiring
higher power than is desirable. Moreover, considering oversampling interpolations on the
15   order of n = 256 for high sampling rates, such as the 400M samples/sec required for
cellular base station applications, extreme clocking speeds (400MHz x 256) become a
serious design obstacle.

Thus, there exists a need for a wireless communications apparatus and
20   corresponding system having an improved DAC operable at higher speed than heretofore
achievable which exploits the sigma-delta principle in a different way.

Summary of the Invention

25

The invention comprises a wireless communications apparatus and corresponding
system having an improved DAC operable at higher speed than heretofore achievable
which exploits the sigma-delta principle in a different way. More particularly, the
invention comprises a wireless user terminal and corresponding system that implement a
30   digital-to-analog conversion circuit having a memory for storing delta-sigma bit
sequences corresponding to all possible values of a digital input coupled to a plurality of
one-bit digital to analog converters. Each of the digital-to-analog converters being
clocked by multi-phase clocks such that each phase applied to each one of the digital to
analog converter is delayed with respect to a next one by the oversampling period, which

5 is the Nyquist period divided by the number of predetermined interpolated samples. An analog summer is coupled to all the digital-to-analog converters for summing all the outputs from the plurality of digital to analog converters to generate an analog output. Hereby, the digital-to-analog conversion circuit embodied in the wireless communications apparatus and corresponding system emulates a delta-sigma digital-to-
10 analog converter having both high speed and high resolution.

Brief Description of the Drawings

15 For a more complete understanding of the present invention and the advantages thereof, reference is now made to the following description taken in conjunction with the accompanying drawings in which like reference numbers indicate like features and wherein:

Figure 1 is a schematic of a known first order sigma-delta converter;

20 Figure 2 is a schematic of a known second order sigma-delta converter;

Figure 3 shows a known over-sampling DAC system having the known first order sigma-delta converter of FIG. 1;

Figure 4 illustrates the prior art digital signal processor and DAC arrangement;

Figure 5 illustrates a first order sigma-delta converter coupled to a read only
25 memory to program;

Figure 6 illustrates an embodiment of a sigma-delta modulator as disclosed in one embodiment of the present invention;

Figure 7 shows the timing diagram of the clocking signals for each one-bit DAC in the sigma-delta modulator in accordance with the present invention;

30 Figure 8 displays a flow chart of the method of modulating a signal in accordance with the present invention;

Figure 9 illustrates a communications system that implements the sigma-delta modulator of one embodiment of the present invention;

5   Figure 10 illustrates a block diagram of a wireless user terminal implemented in an embodiment of the present invention;

        Figure 11 illustrates a wireless user terminal block diagram that implements the sigma-delta modulator according to an embodiment of the present invention;

10   Figure 12 illustrates a wireless user terminal receiver block diagram that implements the sigma-delta modulator according to an embodiment of the present invention;

        Figure 13 illustrates the transmitted spectra for TDMA (GSM) and CDMA (IS-95)

15   systems; and

        Figure 14 illustrates a spectral definition of 2G and 3G cellular regulations.

20   **Detailed Description of Preferred Embodiments**

        The present invention is best understood by comparison with the prior art. Hence, this detailed description begins with a discussion of a well-known first order sigma-delta quantizer, as shown in Figure 1. The purpose of this quantizer in a D/A converter is to

25   convert a high-resolution digital signal x_i, 11, having several bits (16, for example) into a single-bit code y_i, 12, which can be accurately converted to analog. Input 11 is fed to the quantizer 21 via an integrator 16, and quantized output 12 is fed back as feedback 25 and subtracted using adder 14 from the input. Quantizer 21 generates a 1-bit output depending upon whether the output of the integrator is positive or negative. The quantizer function

30   is modeled as adding the output of integrator 16 to an error signal e_i (not shown). This modeling allows the calculation of the spectrum of the noise to be done in a straightforward manner.

5   For large positive inputs, the integrator output will be positive. A logic one is then the output of the quantizer, which is fed back and subtracted from the input. The series of output ones continues until the integrator output, which is ramping down due to the negative feedback, finally crosses the quantizer threshold, at which point the quantizer outputs a negative one. Over time, the average output y_i equals the input x_i. The system

10   is called a first order sigma-delta converter, because a single integrator stage is used.

Figure 2 shows a common second order sigma-delta quantizer. In many D/A conversion applications, sigma-delta modulators are chosen to be at least second order because higher order modulators better reduce noise in the signal band, due to improved

15   prediction of the in-band quantization error. Thus, the resulting signal-to-noise ratio is better. Second order sigma-delta modulators are still relatively stable and easy to design. However, third and higher order modulator design can become quite complex.

For the quantizer of Figure 2, input x_i 30, is added to feedback signal 42 by

20   adder 32. The signal from adder 32 is fed into first accumulator 34. The output of accumulator 34 is fed into second accumulator 36. The output of accumulator 36 goes into quantizer 38. The residue or error signal e_i (not shown) is added to the input x_i by adder 32. Quantized output 38 also feeds back as feedback signal 42. Quantizer 38 may quantize the signal into ones and zeroes (1-bit format) or into multiple levels.

25

For simplicity, oversampling by repeating the input data at higher frequencies is considered. The analysis of a delta-sigma loop with constant input is simple. It can be assumed that the residue R output of the integrator 16 in Figure 1 remains bounded to a small value (denoted by ε because of the negative feedback around the loop). The residue

30   R is equal to the error in the input sequence x_i minus the output sequence y_i, as follows:

$$\sum (x_i - y_i) = R \rightarrow \varepsilon$$

5   For n times oversampling using repetition of the input data n times between Nyquist samples, since x_i is constant for the n iterations, after n iterations of the loop, this error reduces to ε/n.

$$\sum x_i \cdot \sum y_i = \varepsilon$$
$$n\sum x \cdot \sum y_i = \varepsilon$$
$$x = (1/n)\sum y_i + (1/n)\,\varepsilon$$

10

In a second order loop, there are two integrators in tandem. The input gets accumulated as x, 2x, 3x, .. nx in the first integrator. In turn, the second integrator will contain as x, 3x, 6x, .. $n(n+1)x/2$ due to the input samples alone. Thus, the error goes down in a quadratic fashion as $2/(n^2+n)$.

15

$$\sum\sum x_i \cdot \sum\sum y_i = \varepsilon$$
$$\{n(n-1)/2\}\sum\sum x \cdot \sum\sum y_i = \varepsilon$$
$$x = (2/(n^2+n))\sum\sum y_i + (2/(n^2+n))\,\varepsilon$$

In other words, by increasing the order of the loop or n, one can make the error negligibly small as the stored value grows in proportion to n.

20

As disclosed in U. S. Patent No. 5,815,102, which is incorporated by reference herein, Figure 3 shows an oversampling D/A converter which utilizes a second order sigma-delta quantizer 70 and a one-bit D/A converter 71 as the demodulator 69, and a low pass filter 73 to remove the noise from the 1-bit signal. Oversampling is used to

25   increase resolution by reducing quantization error to a small value. Techniques for increasing the sample rate, generally called interpolation, are well understood by those versed in the art. Typical techniques, among many, include zero stuffing and data repetition.

5   In Figure 3, the input signal x_i, 60, consists of data encoded into 16-bit words at 8 kHz. These words are placed into a register 63 from which they are fed into a low pass filter 64 at 32 kHz, with each word repeated four times. The low pass filter is of the finite impulse response type. The linear interpolator 66, which is also a low pass filter, inserts three new words between each pair of words from low pass filter 64, which raises the data

10   rate to 128 kHz. These words are fed into a second register 67, which feeds each word into the demodulator 69, repeating each word eight times, resulting in a data rate of 1 MHz. This repeating of the samples is a simple type of low pass filter. The 1 MHz sample rate is a sufficiently high data rate for audio applications so that the quantization noise which will be introduced into the signal is small, and the requirements of the analog

15   smoothing filter are easily met. Output y_i, 61, is an analog signal. For audio applications, the output of demodulator 69 can sometimes be driven directly into a speaker, because the speaker can act as a low pass filter. This configuration uses what is called class D output or pulse density modulation drive. Power dissipation in a class D stage has the potential for being very low, as the output transistors are always in either a fully shorted or open

20   position, removing most resistive power consumption.

       An oversampling D/A converter like that of Figure 3, which utilizes a second order sigma-delta quantizer 70, and a low pass filter 71 to convert the data from the sigma-delta quantizer 70 to analog signal y_i, 61, is a very effective device for low speed

25   sampling such as for low speed audio applications. However, it has a relatively high output data transition rate, requiring higher power than is desirable. Moreover, at high speed sampling rates, such as the, for example, 200MHz sampling required for cellular base station applications, and oversampling interpolations on the order of n = 256 times oversampling, extreme clocking speeds (400MHz x 256) becomes a serious design

30   obstacle.

       Oversampling may be achieved by any given interpolation procedure. For example, where over-sampling is performed on a sample which is held constant for a whole Nyquist period, the interpolation reduces to repeating the input sample value n-

5   times where n is the oversampling ratio. A sample and hold operation results in a low-pass filtering function and this is the well known (sinX)/X function. Figure 4 shows a known implementation using a digital signal processor 80 coupled to the an oversampling sigma-delta modulator. The digital signal processor calculates the sequence values with the incoming signal in real time and the sigma-delta converter operates at oversampling

10   rate. This, however, turns out to be an unnecessary and power-hungry operation.

Figure 5 illustrates the apparatus used which provide off-line processing of output sequences in accordance with the present invention. A 16-bit input word is received by a sigma-delta converter 100 that is coupled to a read-only memory 110. The input signal

15   and the output signal of the sigma-delta converter 100 are coupled to the read-only memory 110 to be stored as a table. In operation, sigma delta conversion pre-calculated off-line to generate the output sequence as well as residue if not negligible. This becomes possible since the conversion of one value of the signal is independent of the previous history of the inputs. Thus, the 65,536 values corresponding to all possible 16-bit inputs

20   can be fed on a one-at-a-time basis into the off-line sigma delta converter. The converter runs for n cycles where n is the oversampling factor. The output sequence of n bits and residue obtained from this off-line computation are stored in a read-only memory 110 addressable by a 16-bit input word.

25   Figure 6 displays a high speed, high-resolution digital-to-analog converter 105 in accordance with the present invention. A 16-bit input word at the input signal 106 addresses the read-only memory 110 of Figure 5 that contains the pre-computed delta-sigma values corresponding to all possible 16-bit inputs. The values stored in the read-only memory 110 when addressed by the input signal 106 will output all the stored values

30   of the sigma delta sequence simultaneously. The output can be converted to the required analog signal by using a plurality of one bit digital to analog converters (DACs) 120, 122, 124 and 126 coupled to the n outputs of ROM 110, each clocked by multi-phase clocks each delayed with respect to the next by the oversampling period. The data stored in ROM 110 is compressed if necessary to minimize the number of storage cells or size of

5   the ROM 110. Depending upon what is stored in ROM 110, the data output from the ROM 110 may be in variety of useful, low transition rate formats.

Given a delay-lock loop and n one-bit DAC's 120, 122, 124 and 126, when the memory is addressed by an input, the whole stored bit-sequence as well as the residue is
10   transferred to the output simultaneously. The sequence is stored as a column, these bits are fed to the DAC's 120, 122, 124 and 126 in parallel as shown. Each DAC 120, 122, 124 and 126 may be implemented using a current steering arrangement having a single differential pair and a tail current source. Each differential pair is switched by a clocked flip-flop thereby transferring current from one side to the other. The DAC's 120, 122,
15   124 and 126 are clocked with delayed clocks shown in Figure 7. The delay between adjacent clocks is the T/n where T is the Nyquist period. This multi-phase clock must be obtained using a delay-lock loop with very low jitter. For improved accuracy reasons, if stored residues are outputted, a separate residue adder 128 and DAC 130 will be necessary. These values will be added in the digital domain. Only when the value of the
20   residue becomes appreciable (i.e. when the most significant bit becomes one) will it be converted to analog and added to the output as a correction.

The analog output obtained by summing all the DAC 120, 122, 124 and 126 outputs then emulates a sigma-delta DAC yet this embodiment provides both high speed
25   and high resolution not possible by prior art sigma-delta solutions. Note that this output has shaped quantization-noise at high frequencies above the oversampling rate that must be filtered out. A convenient way to do this, as disclosed in U. S. Patent No. 5,012,245 (which is incorporated herein), is to use an FIR filtering technique which is obtained simply by adjusting the tail currents of the various DAC's 120, 122, 124 and 126 to
30   correspond to the coefficients of the filter. Multiplication is trivial when one of the operands is a +1, -1 or 0. Note that inaccuracies in coefficients of the filter will not introduce non-linearity or spurs but will only change the frequency response of the filter.

5   Another embodiment may include the incorporation of a second-order sigma-delta loop, to obtain 100 dB dynamic range, the oversampling ratio is 128. This means that the read-only store is 65K x 128 bits. If a higher order loop or a multi-bit delay loop is utilized, the oversampling ratio will be smaller; however, the DAC 105 becomes more complex although the number of DAC's 120, 122, 124 and 126 as well as the number of

10   clock-phases reduces.

       Still another embodiment may include an apparatus to apply the optimum number of taps and the tap weight coefficients of the filter. The method of designing the optimum number of taps and the tap weight coefficients as disclosed in U. S. Patent

15   No. 5,012,245 are incorporated herein. Specifically, these tap weight coefficients would be applied to the analog output signals from the DAC's 120, 122, 124 and 126.

       Yet another embodiment may include a ROM such as the one in Figure 5 where the data is compressed taking advantage of symmetry in the table and then stored. The

20   data is later expanded by an expansion unit coupled to the output of the ROM after it leaves the ROM in Figure 6. The corresponding expansion unit must be at a high speed as well.

       A sub-assembly may be comprised solely of the ROM having the pre-stored sigma

25   delta digital sequence for possible values of digital input.

       A method of converting a digital signal to an analog signal having high speed and resolution is summarized in the flow chart of Figure 8. At the start (step 200), sigma-delta analog sequence patterns are generated off-line for all possible digital signal inputs

30   as shown in step 201. These sequence patterns are stored in a storage means such as a read-only memory in step 202. After a digital signal input addresses the read-only memory to retrieve the stored sequence pattern in step 203, the analog sequence pattern is retrieved in step 204. This data is applied to a plurality of digital-to-analog converters in step 205. In step 206, each of the plurality of digital-to-analog converters is clocked by a

--11--

5   multiphase clock. All the outputs from each digital-to-analog converter are summed to present an output signal in step 207, which ends the process (step 208).

       The high speed, high-resolution digital-to-analog converter of the present invention can be used in a variety of telecommunication and other applications.
10   Conveniently, digital-to-analog converter 105 can be part of wireless user terminals and base stations operating according to international standards, such as for example CDMA (Code Division Multiple Access) and GSM (Global System for Mobile Communication).

       Figure 9 illustrates a wireless communication system in which the digital-to-
15   analog converter of the present invention may be implemented. Wireless communication system 300 comprises a wireless user terminal (a cellular handset being illustrated) 302 that communicates with a base station (a cellular base station being illustrated) 304 over an uplink channel 306 and downlink channel 308. The base station and the wireless user terminal unit operate in a similar manner.
20

       Cellular communication in system 300 can be facilitated in Time Domain Duplex (TDD) or in Frequency Domain Duplex (FDD). In Time Domain Duplex (TDD) the communication between wireless user terminal 302 and base station 304 is on a single channel. Much like a walky-talky, the channel is shared in time by the mobile station
25   transmitter and the base station transmitter. A time slot is dedicated to the uplink and another timeslot is dedicated to a downlink. The relative length of the uplink and downlink time slots can be adjusted to accommodate asymmetric data traffic. If it is found that downlink data traffic is on average twice that of uplink, then the downlink time slot is twice as long as the uplink time slot. In Frequency Domain Duplex (FDD) the
30   wireless user terminal 302 and the base station 304 communicate over a pair of radio frequencies. The lower frequency is the uplink during which the mobile station sends information to the base station. Both uplink and downlink are each composed of a signal source, a transmitter, the propagation path, a receiver and a method of presenting the information. Both wireless user terminal and base station embody the invention with

5   transmitters, which convert digital data to analog signals at high speed and with high resolution. The base station could convert the entire multi-carrier downlink signal to analog for use in a single RF transmitter. The wireless user terminal is explained in the following.

10   Figure 10 presents a top-level block diagram 310 of the wireless user terminal 302. In wireless user terminal 302, radio frequency (RF) signals are received and transmitted by the RF section 312. In the embodiment illustrated, RF section 312 comprises a duplexer 335 coupling an antenna 338 to a receiver 317 and a power amplifier 323. A modulator 321 is coupled to power amplifier 323 and to a synthesizer

15   319. Synthesizer 319 is further coupled to receiver 317. RF section 312 is further coupled to an analog baseband 313. In the embodiment illustrated, analog baseband 313 comprises an RF interface 314 and an audio interface 315. A speaker 337 and a microphone 339 are coupled to audio interface 315. RF interface 314 is coupled to both receiver 317 and modulator 321 of RF section 312. The analog RF interface 314 includes

20   I and Q analog-to-digital converters (ADCs) and digital-to-analog converters (DACs) 105 for conversion between the analog and digital domains. Audio interface 315 may also include I and Q analog-to-digital converters (ADCs) and digital-to-analog converters (DACs) 105 for conversion between the digital and analog domains. Analog baseband 313 is further coupled to a digital baseband 316.

25

      In the illustrated embodiment, digital baseband 316 comprises three elements: digital signal processor (DSP) 318, microcontroller unit (MCU) 320 and application specific integrated circuit (ASIC) 322. DSP 318 couples audio interface 315 to RF interface 314 and to microcontroller unit (MCU) 320. Digital signal processor (DSP) 318

30   and microcontroller unit (MCU) 320 are further coupled to ASIC backplane 322. Microcontroller unit (MCU) 320 is further coupled to a user interface 327, which comprises at least a user display 329 and a keyboard 331 (an optional SIM card 333 is also disclosed).

5   The digital signal processor (DSP) 318, provides programmable speech coding and decoding (vocoder), channel coding and decoding, equalization, demodulation and encryption. The microcontroller unit (MCU) handles level 2 & 3 protocol, radio resource management, short message services, man-machine interface and the real-time operating system. The ASIC backplane 322 performs all chip-rate processing. While top level

10 diagram 310 illustrates RF section 312, analog baseband 313 and digital baseband 316 as being separate packages or chips, the invention contemplates substitution of any of the above with an equivalent function, such as an RF function, and/or an analog baseband function and/or a digital baseband function. The functions will remain the same even if the actual implementation varies. The invention further contemplates that RF section

15 312, analog baseband 313 and digital baseband 316 may be selectively combined and/or integrated into one or two packages or chips.

         An uplink voice processing chain 306 for a wireless user terminal 302 is illustrated in Figure 11. This channel includes a CODEC 345 coupling a microphone 339

20 to a vocoder 343, a baseband modulator 341 coupling vocoder 343 to a digital-to-analog converter 325 at high speed and high resolution. An RF transmitter 334 (part of RF section 312) couples an antenna 338 to digital-to-analog converter 325. Within RF transmitter 334, modulator 321 is implemented as two RF mixers, I and Q driven by the synthesizer, implemented as an RF local oscillator. RF transmitter CODEC 345 includes

25 an audio amplifier (not shown), sigma-delta analog-to-digital converter (ADC) (not shown) and a digital filter (not shown) coupled together on one chip. The CODEC receives an analog voice signal through the microphone and converts it to a digital signal. While CODEC 345 is shown as being separate from digital baseband 316, it may also be internal to digital baseband 316. CODEC 345 transcodes audio signals into digital words

30 using the algorithms contained in the VOCODER. This signal is then complex modulated, converted to analog (I&Q) and applied to the transmitter. The transmitter is complex modulated at the radio frequency assigned to the handset. It uses a power amplifier coupled to the antenna 338 to transmit the digital signal, effectively communicating the (digital) voice information to the base station receiver.

5   A downlink voice channel 308 for wireless user terminal 302 is illustrated in Figure 12. This channel includes an RF receiver 340 (part of RF section 312) coupling antenna 338 to a analog-to-digital converter (ADC) 342 (while a sigma-delta analog-to-digital converter (ADC) is shown in the embodiment of Figure 12, other analog-to-digital

10   converters can be used), a vocoder 343 coupling a demodulator 344 to a CODEC 345, and a speaker 337 coupled to CODEC 345. While CODEC 345 is shown as being separate from digital baseband 316, it may also be internal to digital baseband 316. CODEC 345 transcodes the digital words into analog signals using the algorithms contained in the VOCODER. CODEC 345 includes a digital filter, DAC and audio

15   amplifier coupled together on one chip. The RF receiver uses an AGC circuit which varies the IF amplifier gain as a function of the received signal. The goal is to present the analog-to-digital converters (ADCs) with a full-scale analog signal without distortion and with minimal noise.

20   The band structure of the cellular system in which the communication system of the present invention operates is composed of tightly packed RF carriers with very high spectral density. As illustrated in Figure 13, the world's most widely deployed TDMA system is GSM, where the GMSK-modulated carriers are placed on a 200-Khz raster 348 with adjacent channel signal interference suppressed to -30dBc at the first adjacent

25   channel and -60dBc at the second. The 2-G CDMA system used in America (IS-95) uses QPSK-modulated (at 1.2288 Msps) carriers spaced at 1.25 Mhz 350 with very little guard band. Each carrier can be modulated with up to 32 Walsh codes, which are used to separate the users. As previously mentioned, using high speed, higher resolution digital-to-analog converters (DACs) disclosed in this invention, enables multi-carrier base

30   station transmission through a common RF power amplifier.

       Figure 14 illustrates the spectral definition of the 2G and 3G cellular regulations. The base station transmitter operates on the upper frequency band. For example, in

5   Europe the base station receives from 1900 to 1980 Mhz and transmits from 2110 to 2170 Mhz.

The digital-to-analog converter of the present invention can be use in other applications, such as data communication systems, hard disk drives, cd players, video

10   displays, and any other application where there is a large amount of data that must be converted quickly.

The terms and expressions which have been employed in the foregoing specification are used therein as terms of description and not of limitation, and there is no

15   intention in the use of such terms and expressions of excluding equivalents of the features shown and described or portions thereof, it being recognized that the scope of the invention is defined and limited only by the claims which follow.